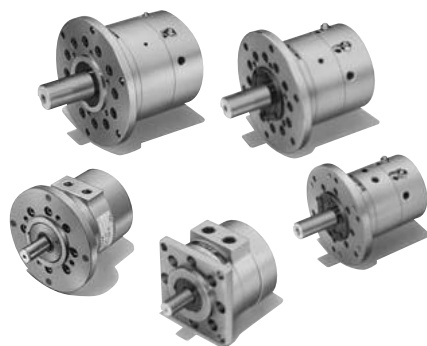


Vane type actuators with max. working pressure of 7 MPa

- Single vane and double vane type rotary actuators are standardized.
- Available the cushion model.
- The shaft parallel key (single key) .



Specifications: Standard type

Item Model	Vane type	Rotating angle	Port size	Internal volume cm ³	Internal leakage rate cm ³ /min (at 40°C)	Allowable inertia energy J	Allowable load		Weight kg	Remarks	
							Radial load	Thrust load			
70RV 10	Single	270° $^{+3}_0$	Rc1/8	10	10	0.013	9.81	4.90	1	Standard	
	Double	90° $^{+3}_0$		6.5	20						
70RV 15	Single	270° $^{+3}_0$	Rc1/8	17	15	0.025	19.6	9.81	2		
	Double	90° $^{+3}_0$		11	30						
70RV 20	Single	270° $^{+3}_0$	Rc1/8	24	20	0.046	49.0	24.5	3		
	Double	90° $^{+3}_0$		16	40						
70RV 30	Single	270° $^{+3}_0$	Rc1/8	51	30	0.088	78.5	39.2	4.3		
	Double	90° $^{+3}_0$		34	60						4.5
70RV 100	Single	270° $^{+3}_0$	Rc1/4	111	50	0.255	147	68.6	10.2		
	Double	90° $^{+3}_0$		74	100						10.4
70RV 200	Single	270° $^{+3}_0$	Rc3/8	221	100	0.510	294	137	20.0		Order made
	Double	90° $^{+3}_0$		147	200						
70RV 400	Single	270° $^{+3}_0$	Rc3/8	435	100	0.755	343	167	32		
	Double	90° $^{+3}_0$		290	200					33	
70RV 700	Single	270° $^{+3}_0$	Rc1/2	780	100	0.912	343	167	41		
	Double	90° $^{+3}_0$		520	200					43	

Common conditions

- Adaptable fluids: Petroleum-based fluid (When using another fluid, specify the fluid.) Recommended fluid: ISO VG32 to 56 (ISO viscosity grade)
- Nominal pressure: 7 MPa
- Minimum operating pressure: 1 MPa
- Proof test pressure: 10.5 MPa
- Hydraulic fluid temperature: 0 to +60°C (No freezing)
- Use the actuators indoors.
- Do not use them in a place where they are exposed to considerable dust or vibration.

(Notes) ● For the internal structure, refer to the sectional drawings at the end of this catalog.

- The hydraulic pressure generated in an actuator due to the inertia of load must be lower than the proof test pressure.

Adaptability of Fluid

Adaptable fluid				
Petroleum-based fluid	Water-glycol fluid	Phosphate ester fluid	Water in oil fluid	Oil in water fluid
○	○	×	×	×

Specifications: With cushion

Item Model	Vane type	Rotating angle	Port size	Internal volume cm ³	Internal leakage rate cm ³ /min (at 40°C)	Allowable load		Weight kg
						Radial load	Thrust load	
70RV 10	Single	180° $^{+3}_0$	Rc1/8	6.5	10	9.81	4.90	1.2
		90° $^{+3}_0$		3.3				
70RV 15	Single	180° $^{+3}_0$	Rc1/8	11	15	19.6	9.81	2.4
		90° $^{+3}_0$		5.5				
70RV 20	Single	180° $^{+3}_0$	Rc1/8	16	20	49.0	24.5	3.3
		90° $^{+3}_0$		8				
70RV 30	Single	180° $^{+3}_0$	Rc1/8	34	30	78.5	39.2	4.7
		90° $^{+3}_0$		17				
70RV 100	Single	180° $^{+3}_0$	Rc1/4	74	50	147	68.6	13.5
		90° $^{+3}_0$		37				
70RV 200	Single	180° $^{+3}_0$	Rc3/8	147	100	294	137	25.7
		90° $^{+3}_0$		73.5				
70RV 400	Single	180° $^{+3}_0$	Rc3/8	290	100	343	167	34
		90° $^{+3}_0$		145				
70RV 700	Single	180° $^{+3}_0$	Rc1/2	520	100	343	167	44
		90° $^{+3}_0$		260				

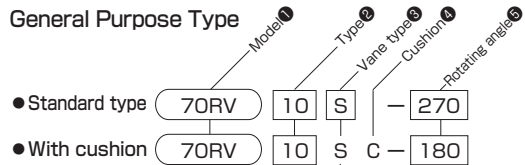
Cushion Specifications

Item Model	Max. inertia moment kg·m ²	Max. inrush angular speed rad/s	Cushion angle rad	Max. absorbed energy					
				Working pressure MPa					
				2	3	4	5	6	7
70RV 10	0.098	10.4	0.349(20°)	2.06	1.77	1.47	1.18	0.883	0.588
70RV 15	0.196	10.4	0.436(25°)	4.81	4.12	3.43	2.75	2.06	1.37
70RV 20	0.294	10.4	0.436(25°)	7.55	6.47	5.39	4.31	3.24	2.16
70RV 30	0.588	10.4	0.436(25°)	15.1	12.9	10.8	8.63	6.47	4.31
70RV 100	1.47	8.7	0.436(25°)	30.9	26.5	22.1	17.7	13.2	8.83
70RV 200	3.92	6.9	0.436(25°)	78.9	67.7	56.4	45.1	33.8	22.6
70RV 400	6.86	5.2	0.436(25°)	137	118	98.1	78.5	58.8	39.2
70RV 700	13.7	4.3	0.436(25°)	251	215	179	143	107	71.6

(Note) From the viewpoint of the torque efficiency, the working pressure should be 2 MPa or more. If the actuator is used at a pressure of less than 2 MPa for unavoidable reasons, the max. absorbed energy is the same as that at a working pressure of 2 MPa.

● How to order

General Purpose Type



Standard type
10·15·20·30·100·200·400·700

S Single vane
D Double vane

Standard type

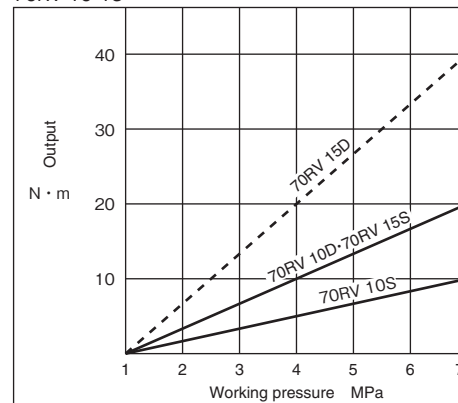
270 270° (only single vane type)
90 90° (only double vane type)

With cushion

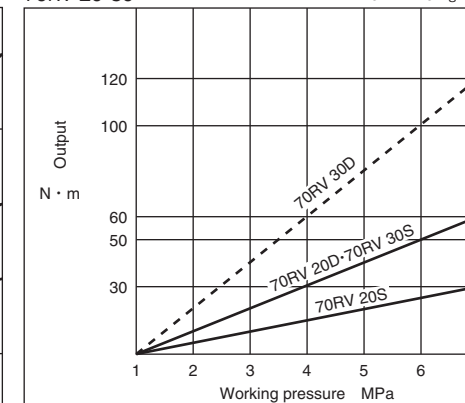
90 90°
180 180°

Output Characteristic Charts (Theoretical torque)

70RV 10·15

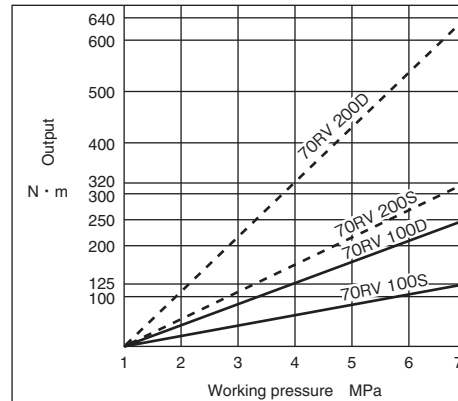


70RV 20·30

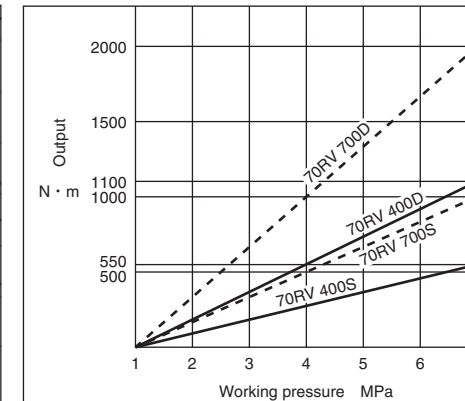


1MPa=10.2kgf/cm²
10N·m=1.02kgf·m

70RV 100·200



70RV 400·700



● These charts are common to the standard type and the type with cushion.

CAD/DATA is available.

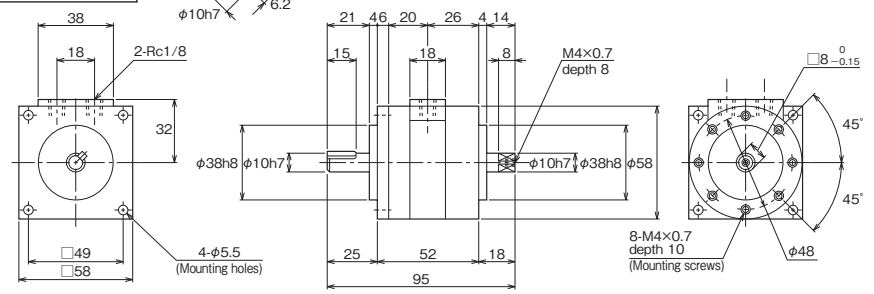
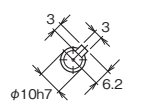
70RV/T70RV is available.

●The tolerances of the dimensions of the key conform to JIS B1301.

70RV 10 * - *

Vane type
S: Single
D: Double
Rotating angle
270° (only single vane type)
90° (only double vane type)

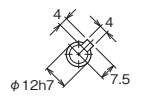
Dimensions of key



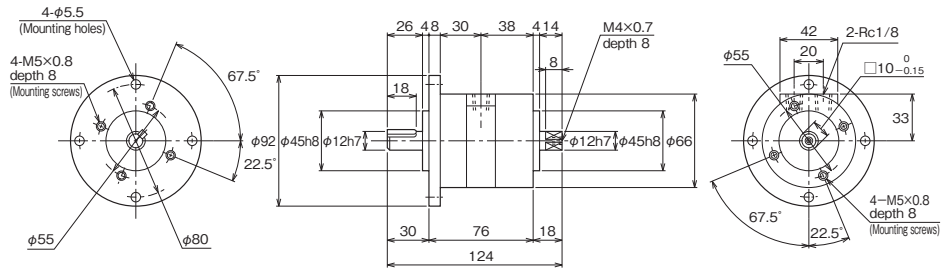
70RV 15 * - *

Vane type
S: Single
D: Double
Rotating angle
270° (only single vane type)
90° (only double vane type)

Dimensions of key



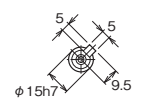
●The tolerances of the dimensions of the key conform to JIS B1301.



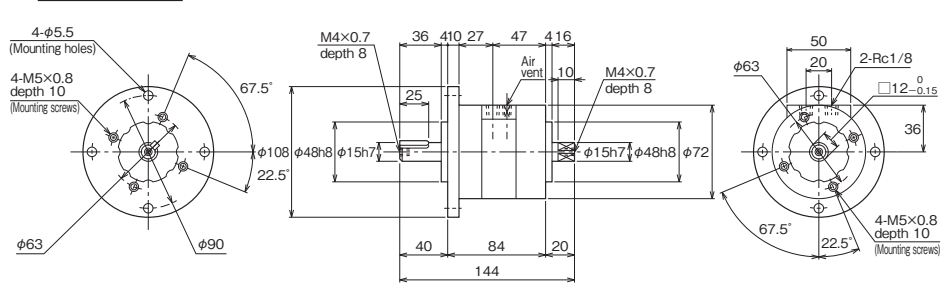
70RV 20 * - *

Vane type
S: Single
D: Double
Rotating angle
270° (only single vane type)
90° (only double vane type)

Dimensions of key



●The tolerances of the dimensions of the key conform to JIS B1301.



CAD/DATA is available.

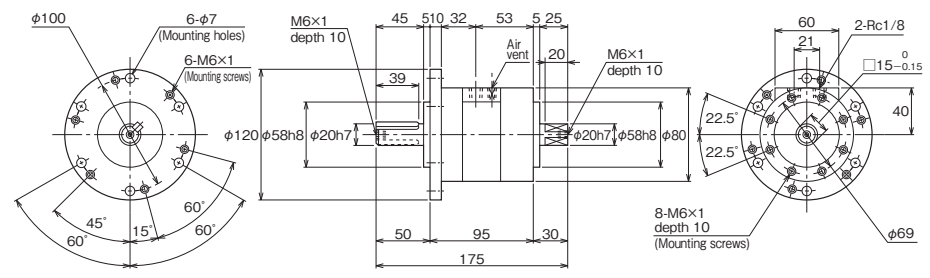
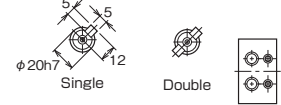
70RV/T70RV is available.

●The tolerances of the dimensions of the key conform to JIS B1301.
●The double vane type rotary actuator is provided with two parallel keys.

70RV 30 * - *

Vane type
S: Single
D: Double
Rotating angle
270° (only single vane type)
90° (only double vane type)

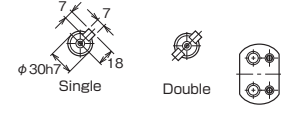
Dimensions of key



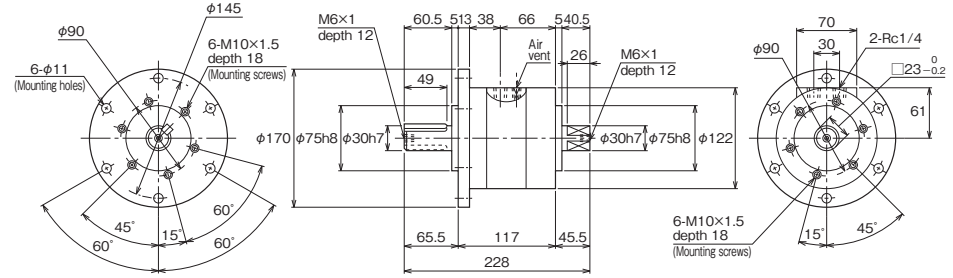
70RV 100 * - *

Vane type
S: Single
D: Double
Rotating angle
270° (only single vane type)
90° (only double vane type)

Dimensions of key



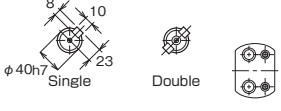
●The tolerances of the dimensions of the key conform to JIS B1301.
●The double vane type rotary actuator is provided with two parallel keys.



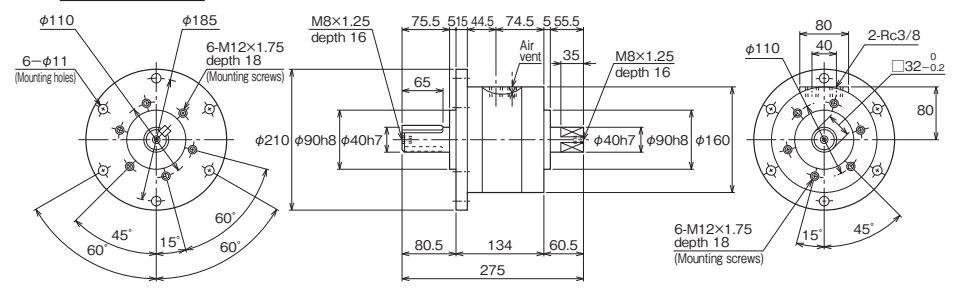
70RV 200 * - *

Vane type
S: Single
D: Double
Rotating angle
270° (only single vane type)
90° (only double vane type)

Dimensions of key

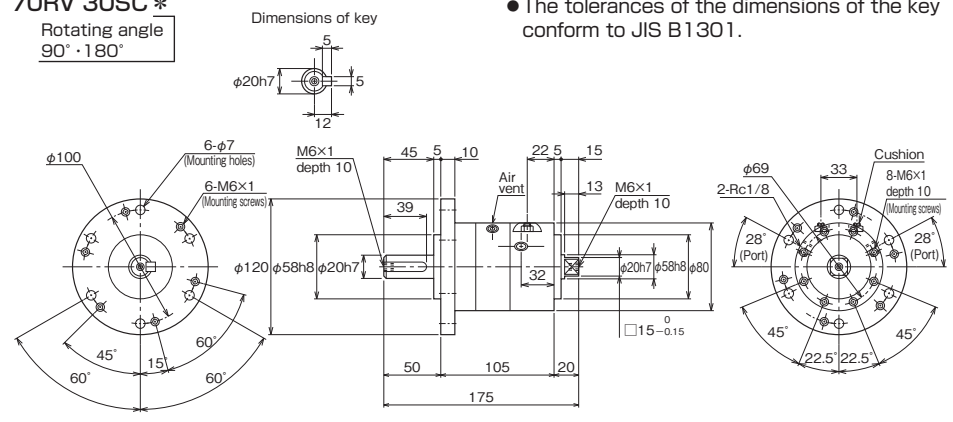


●The tolerances of the dimensions of the key conform to JIS B1301.
●The double vane type rotary actuator is provided with two parallel keys.

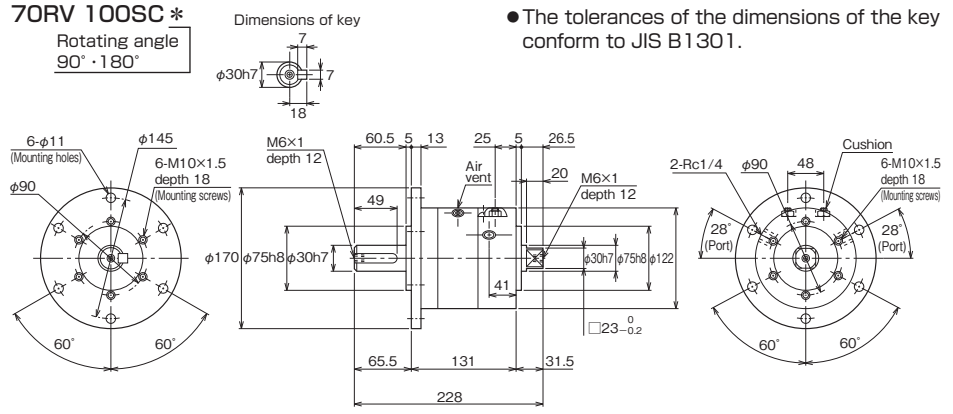


CAD/DATA is available.

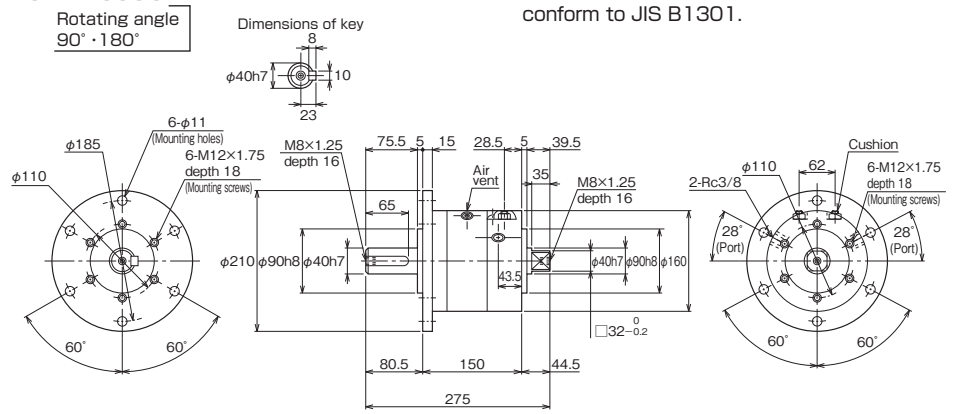
70RV 30SC *
Rotating angle 90° · 180°



70RV 100SC *
Rotating angle 90° · 180°

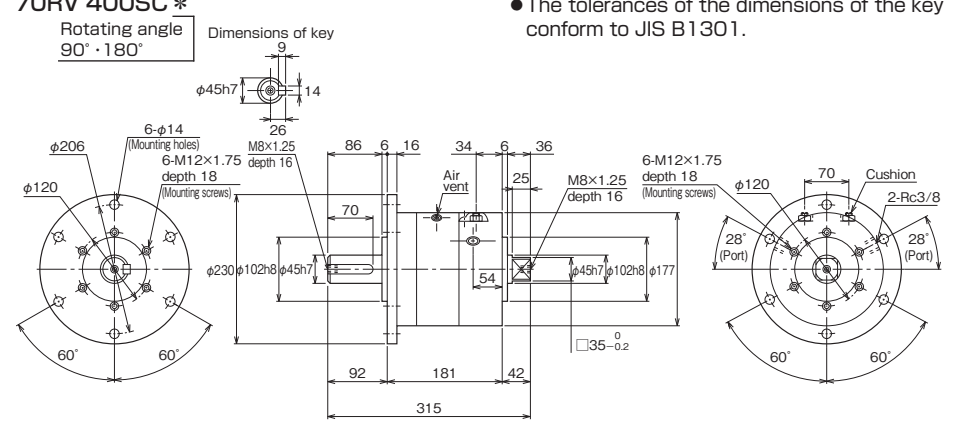


70RV 200SC *
Rotating angle 90° · 180°

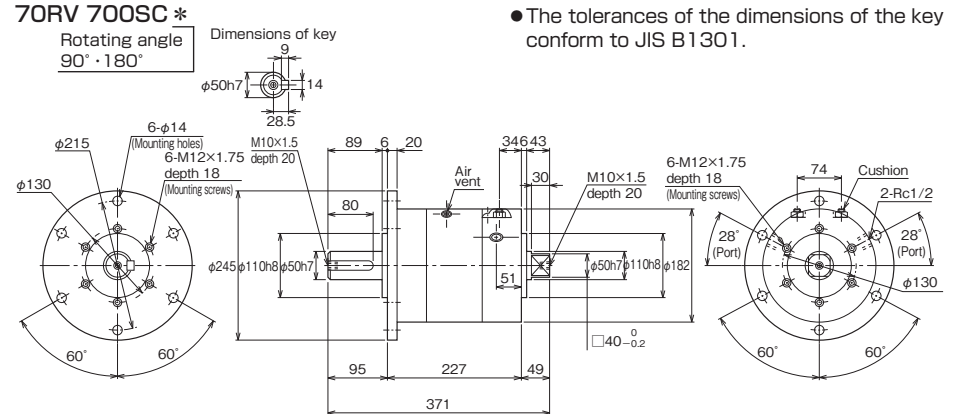


CAD/DATA is available.

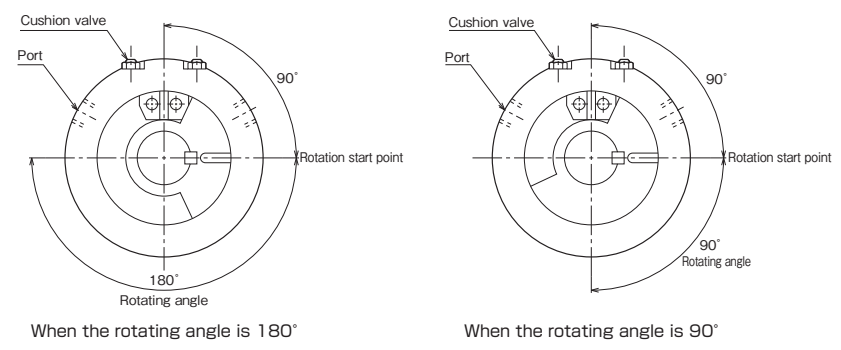
70RV 400SC *
Rotating angle 90° · 180°



70RV 700SC *
Rotating angle 90° · 180°



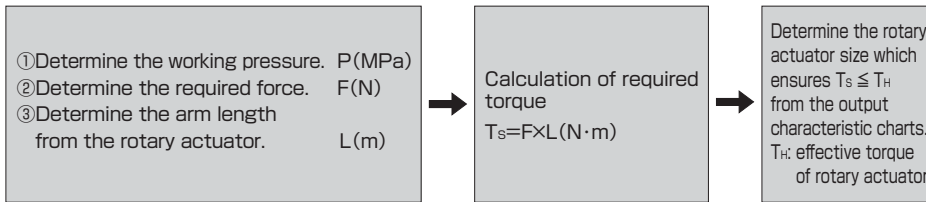
Rotation start point and rotating angle viewed from the front: With cushion



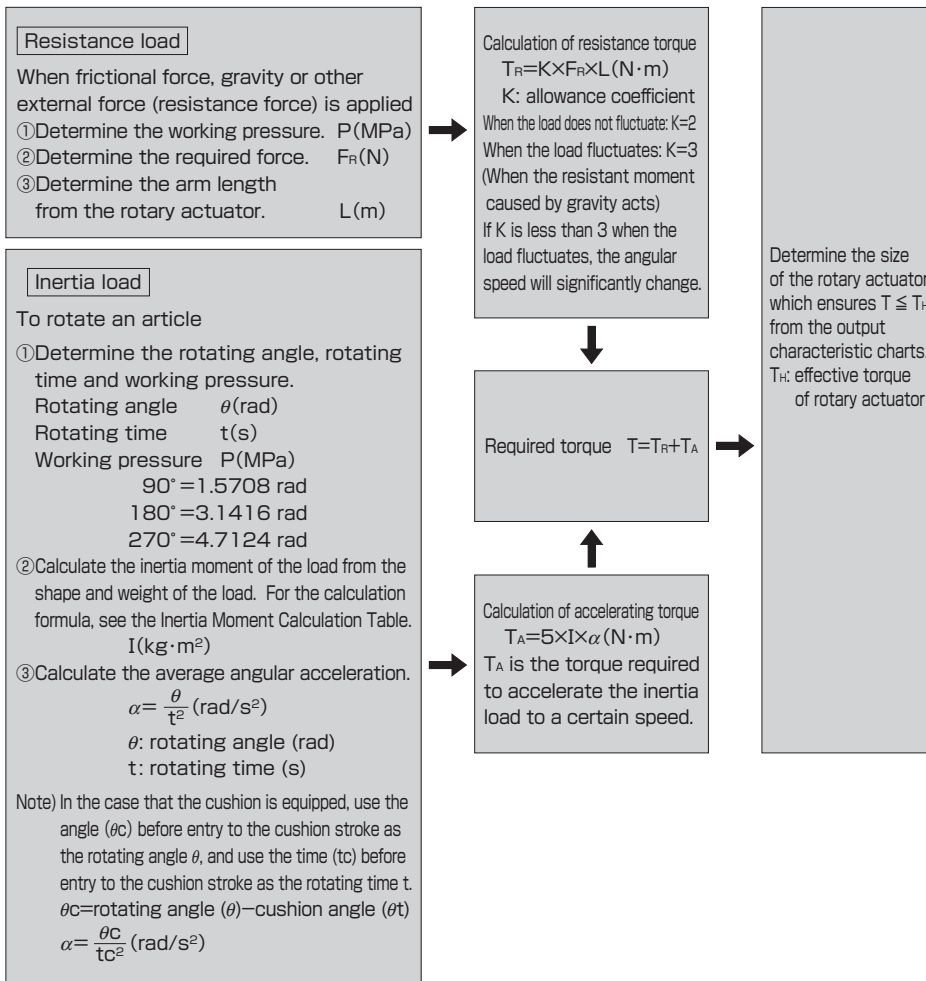
● The position at 90° from the cushion valve (position of the parallel key) is the rotation start point.

1. Selection of size

To obtain simple static force for clamping, etc.



To move a load



2. Check of allowable inertia energy

In the case of inertia load, keep the load inertia energy lower than the allowable inertia energy of the rotary actuator.

- ① Calculation of average angular speed $\omega = \frac{\theta}{t}$ (rad/s)
θ: rotating angle (rad) t: rotating time (s)
- ② Calculate the impact angular speed ω_0
 $\omega_0 = 1.2\omega$ (rad/s)
- ③ Calculation of load inertia energy
 $E = 1/2 I \omega_0^2$ (J)
I: load inertia moment (kg · m²)
- ④ Make sure that the load inertia energy E is less than the allowable inertia energy of the rotary actuator.
If E exceeds the allowable inertia energy, select a larger rotary actuator or a rotary actuator with cushion.

3. Confirmation of cushion performance (in the case of rotary actuator with cushion)

Determine the inertia moment I from the shape and weight of the load, and make sure that the inertia moment is within the load range. $I \leq I_{max}$ I (kg · m²)

Make sure that the impact angular speed for rushing into the cushion is less than the max. impact angular speed.
 $\omega = \frac{\theta_C}{t_C}$ (rad/s) θ_C: angle before entry to cushion stroke (rad)
 $\omega_0 \approx 1.2\omega$ (rad/s) ω₀ ≤ ω_{max} t_C: time before entry to cushion stroke (s)
ω: average angular speed (rad/s)
ω₀: impact angular speed (rad/s)

Determine the impact energy from the load inertia moment and impact angular speed.
 $E_1 = 1/2 I \omega_0^2$ (J) I = inertia moment (kg · m²) ω₀ = impact angular speed (rad/s)

Determine the energy of external force applied during cushion stroke.
 $E_2 = (Mg + Mf) \theta t$ (J) E₂: energy of external force
Mg: gravity moment caused by unbalanced load (N · m)
Mg = L × F_g F_g: force caused by load gravity (N)
In the case of a balanced load or motion on a horizontal surface, Mg = 0.
Mf: moment generated by other thrust forces (for example, when the cylinder force acts) (N · m)
Mf = L × F_f F_f: thrust force (N)
When there are no other thrust forces, Mf = 0.
θt: cushion angle (rad)

Make sure that E₁ + E₂ is less than the max. absorbed energy.

When all requirements stated above are met, the rotary actuator is acceptable. If any of them is not met, the rotary actuator cannot be used. A shock absorber with higher absorbing performance is necessary. See "TAIYO General Catalog of Shock Absorbers".

Inertia Moment Calculation Table

Shape	Sketch	Requirements	Inertia moment I(kg·m ²)	Radius of rotation K _i ²	Remarks
Disc		Diameter d(m) Weight M(kg)	$I=M \cdot \frac{d^2}{8}$	$\frac{d^2}{8}$	
Stepped disc		Diameter d ₁ (m) d ₂ (m) Weight Part d ₁ M ₁ (kg) Part d ₂ M ₂ (kg)	$I=M_1 \cdot \frac{d_1^2}{8} + M_2 \cdot \frac{d_2^2}{8}$		When part d ₂ is significantly small as compared to part d ₁ , it is allowed to ignore d ₂ .
Bar (rotation center at end)		Length of bar l(m) Weight M(kg)	$I=M \cdot \frac{l^2}{3}$	$\frac{l^2}{3}$	When the width of the bar is 30% or more of the length (l), regard the bar as a rectangular solid.
Rectangular solid		Length of side a(m) b(m) Distance to center of gravity l(m) Weight M(kg)	$I=M(l^2 + \frac{a^2+b^2}{12})$	$l^2 + \frac{a^2+b^2}{12}$	
Bar (rotation center at center)		Length of bar l(m) Weight M(kg)	$I=M \cdot \frac{l^2}{12}$	$\frac{l^2}{12}$	When the width of the bar is 30% or more of the length (l), regard the bar as a rectangular solid.
Rectangular solid		Length of side a(m) b(m) Weight M(kg)	$I=M \cdot \frac{a^2+b^2}{12}$	$\frac{a^2+b^2}{12}$	
Lumped load		Shape of lumped load: Disc Diameter of disc d(m) Length of arm l(m) Weight of lumped load M ₁ (kg) Weight of arm M ₂ (kg)	$I=M_1 \cdot l^2 + M_1 \cdot K_i^2 + M_2 \cdot \frac{l^2}{3}$ In case of disc $K_i^2 = \frac{d^2}{8}$		For other shapes, see K _i ² shown above. When M ₂ is significantly small as compared to M ₁ , it is allowed to consider M ₂ to be 0.

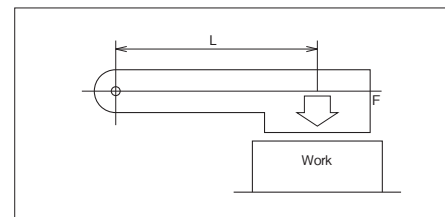
Method of converting load J_L to the load around the rotary actuator axis when a gear is used

Gear		No. of teeth Rotary actuator side a Load side b Inertia moment of load I _L (kg·m ²)	Inertia moment of load around rotary actuator axis $I_H = (\frac{a}{b})^2 I_L$		When the gear is larger, the inertia moment of the gear should be taken into consideration.
------	--	---	---	--	---

Example of selection of vane type rotary actuator

1. To use for a clamp

- Length of arm L=0.2m
- Clamp force F=500N
- Working pressure P=7MPa



To use for a clamp

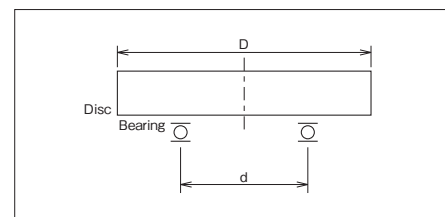
<Selection of size>

Static torque T_S=

According to the Output Characteristic Charts (Theoretical torque), the rotary actuator 70RV-30D or larger model can be used.

2. To rotate a circular table

- Weight of table M=50kg
- Diameter of table D=1m
- Center diameter of plain bearing d=0.3m
- Friction coefficient of plain bearing μ=0.05
- Rotating angle θ=180°
- Rotating time t=3s
- Working pressure P=7MPa



To rotate a circular table

<Selection of size>

① Determine the resistance torque T_R.

T_R=K×F_R×L

Consider that the allowance coefficient K is 2.
Resistance force F_R=μ×M=0.05×50×9.8=24.5(N·m)
Therefore, T_R=2×24.5×0.3/2=7.35(N·m)

② Determine the accelerating torque T_A.

T_A=5×I×α(N·m)

Inertia moment I(kg·m²)

Since the load has the shape of a disc,
I=M·D²/8=50×1²/8=6.25(kg·m²)

Calculation of angular acceleration α(rad/s²)
α=θ/t²=3.1416/3²=0.35(rad/s²)

T_A=5×6.25×0.35=10.94(N·m)

③ Determine the required torque T.

T=T_R+T_A=7.35+10.94=18.29(N·m)

According to the Output Characteristic Charts (Theoretical torque), the rotary actuator 70RV-15S or larger model can be used.

<Check of allowable inertia energy>

① To stop with the stopper in the rotary actuator

Calculation of average angular speed

ω=θ/t=3.141/3=1.05(rad/s)

Calculation of impact angular speed ω₀

ω₀=1.2ω=1.2×1.05=1.26(rad/s)

Calculation of load inertia energy E

E=1/2Iω₀²=1/2×6.25×1.26²=4.96(J)

Judging from the allowable inertia energy, there is no usable rotary actuator.

② To use a cushion

Judging from the max. absorbed energy and max. inertia moment, the rotary actuator 70RV-200SC or larger model can be used.

<Selection of size based on torque and allowable inertia energy>

Use 70RV-100SC, and rotate the load only by the rotary actuator.

<Check of rotating time, radial load and thrust load>

Rotating time: 3 sec

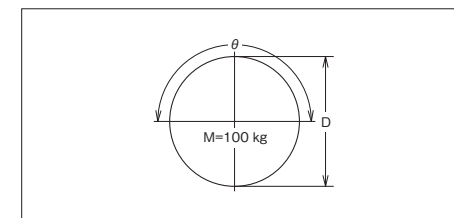
Radial load: 0 kg

Thrust load: 0 kg (because of use of a bearing)

Therefore, the rotary actuator 70RV-200SC or larger model can be used.

3. To rotate a disc

- Weight of disc M=100kg
- Diameter of disc D=0.5m
- Rotating angle θ=180°
- Rotating time t=5s
- Working pressure P=7MPa



To rotate a disc

<Selection of size>

① Determine the resistance torque T_R.

Since no external force acts on the disc, the resistance torque T_R is 0.

② Determine the accelerating torque T_A .

$$T_A = 5 \times I \times \alpha \quad (\text{N} \cdot \text{m})$$

Calculation of inertia moment I ($\text{kg} \cdot \text{m}^2$)

Since the load has the shape of a disc,

$$I = M \cdot D_e^2 / 8 = 100 \times 0.5^2 / 8 = 3.13 \quad (\text{kg} \cdot \text{m}^2)$$

Calculation of angular acceleration α (rad/s^2)

$$\alpha = \theta / t^2 = 3.1416 / 5^2 = 0.13 \quad (\text{rad/s}^2)$$

$$T_A = 5 \times 3.13 \times 0.13 = 2.03 \quad (\text{N} \cdot \text{m})$$

③ Determine the required torque T .

$$T = T_R + T_A = 0 + 2.03 = 2.03 \quad (\text{N} \cdot \text{m})$$

According to the Output Characteristic Charts (Theoretical torque),

the rotary actuator 70RV-10S or larger model can be used.

<Check of allowable energy>

① To stop with the stopper in the rotary actuator

Calculation of average angular speed

$$\omega = \theta / t = 3.1416 / 5 = 0.63 \quad (\text{rad/s})$$

Calculation of impact angular speed ω_0

$$\omega_0 = 1.2 \omega = 1.2 \times 0.63 = 0.76 \quad (\text{rad/s})$$

Calculation of load inertia energy E

$$E = 1/2 I \omega_0^2 = 1/2 \times 3.13 \times 0.76^2 = 0.90 \quad (\text{J})$$

Judging from the allowable inertia energy, the rotary actuator 70RV-700S or larger model can be used.

② To use a cushion

Judging from the max. absorbed energy and max. inertia moment, the rotary actuator 70RV-200SC or larger model can be used.

<Selection of size based on torque and allowable inertia energy>

Use 70RV-400SC, and rotate the load only by the rotary actuator.

<Check of rotating time, radial load and thrust load>

Rotating time 5 sec

Radial load 100 kg

Thrust load 0 kg

Therefore, 70RV-200SC or larger model can be used.

Working Rotating Time

Standard type

Unit: s

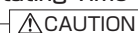
	90°	270°
70RV 10	0.22 to 6	0.54 to 18
70RV 15	0.22 to 6	0.54 to 18
70RV 20	0.23 to 6	0.54 to 18
70RV 30	0.5 to 9	0.54 to 27
70RV 100	0.6 to 9	0.67 to 27
70RV 200	0.75 to 9	0.81 to 27
70RV 400	1 to 18	1.08 to 54
70RV 700	1.8 to 18	1.35 to 54

With cushion (not incl. cushioning zone)

Unit: s

	90°	180°
70RV 10	0.18 to 6	0.36 to 12
70RV 15	0.18 to 6	0.36 to 12
70RV 20	0.18 to 6	0.36 to 12
70RV 30	0.18 to 9	0.36 to 18
70RV 100	0.22 to 9	0.45 to 18
70RV 200	0.27 to 9	0.54 to 18
70RV 400	0.36 to 18	0.72 to 36
70RV 700	0.45 to 18	0.9 to 36

Setting of Rotating Time



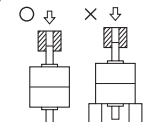
Use the actuator within the range of rotating time shown in the above table. If the rotary actuator is used longer than the above rotating time, smooth operation or cushioning effect cannot be obtained due to stick-slip, etc. If the rotating time is shorter than the above time, the rotary actuator may be damaged.

Precautions for use



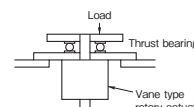
- To install the body, use bolts of strength class 8.8 or over in the specified size. When installing, observe the following instructions.
 - 1) Secure the actuator using all mounting holes.
 - 2) Take care not to tighten the bolts unevenly. Tighten them to the tightening torque specified for the bolts used.
 - 3) Take care not to apply any external load other than the main body load to the bolts. (Use durable mounting materials.)

Fig. 1



- When attaching a load or a joint to the shaft of the vane type rotary actuator, attach it in such a way that its force is not applied to the body as shown in Fig. 1.

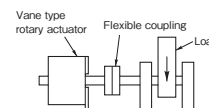
Fig. 2 <Thrust load>



- A load in the axial direction (thrust load) on the shaft of the vane type rotary actuator can cause operation failure. Avoid applying such a load to the actuator. Use a thrust bearing as shown in Fig. 2 so that the thrust load is not applied to the rotary actuator.

- Application of a bending load (radial load) to the shaft end of the vane type rotary actuator can cause operation failure. Avoid applying such a load to the actuator. If this cannot be avoided, provide the rotary actuator with a mechanism as shown in Fig. 3 to convey only the rotating force to the actuator.

Fig. 3 <Radial load>



- When the weight of the load is large and the operating speed is high, shock may be caused by the inertia force, and it may not be absorbed only by the internal shock receiver, thereby resulting in damage to the equipment. In this case, provide a shock absorber to absorb the inertia energy.
- When installing the vane type rotary actuator or starting it after a long-term suspension, discharge air from it. Insufficient discharge of air may cause operation failure.



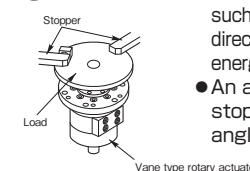
If you have any questions about repair or maintenance, consult us. Never disassemble the actuator.

Notes on piping work

- Take care that dirt and pipe cuttings do not enter the piping.
- Take care that air does not accumulate in the piping.
- When connecting the actuator with a rubber hose, do not bend the hose in a radius lower than the specified radius.
- Be sure to flush the piping. After flushing, connect the piping to the rotary actuator. If the piping is not flushed, contaminants in the piping may cause operation failure of the rotary actuator or fluid leak.
- The vane type rotary actuators cause internal leak. Also, the solenoid valves used on the control circuits cause internal leak. Therefore, they cannot be stopped in the middle of operation under load torque. To suspend any of the actuators in the middle for a long time, provide it with an external mechanical stopper.

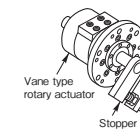
External stopper

Fig. 4



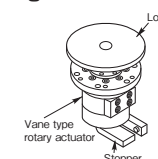
- Attach an external stopper in such a way that the stopper directly receives the inertia energy of the load. (Fig. 4)
- An adjustable external stopper is convenient for angle adjustment.

Fig. 5



- When the actuator must be stopped more accurately, provide an external stopper.
- An adjustable external stopper is convenient for angle adjustment. To ensure the stopping accuracy, it is recommended to attach the stopper to a position with as large radius as possible. (Fig. 5)

Fig. 6

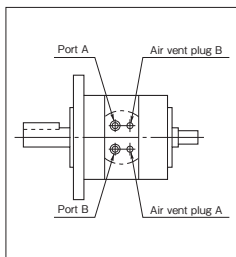


- When the load is driven on the key groove side and an external stopper is provided on the square shaft side, make sure that the load is less than the allowable energy. If the load exceeds the allowable energy, the shaft may be broken. (Fig. 6)

How to discharge air

CAUTION

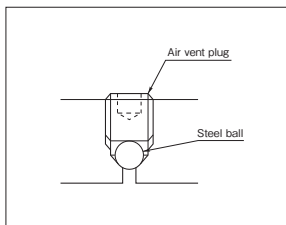
If the air vent plug is loosened excessively, the plug may fly out or the fluid may spout out.



- Feed the fluid at a low pressure to the rotary actuator, and, when the pressure is applied to the port A, loosen the air vent plug A one or two turns (turn counterclockwise) to discharge air.

When the pressure is applied to the port B, loosen the air vent plug B to discharge air.

- If air has accumulated in the rotary actuator, white turbid hydraulic fluid flows out of the air vent plug. Discharge air repeatedly until the white turbidity of the fluid is lost.
- After discharging air, tighten the air vent plug to the specified tightening torque (turn clockwise), and make sure that the fluid does not leak. [Torque: 8 N·m]
- Discharge air not only from the rotary actuator, but also from the piping. If air remains in the piping, operation failure may be caused.
- After discharging air, start the rotary actuator at a reduced pressure, and gradually increase the pressure to the working pressure.
Note) 70RV-10 and 15 do not have air vents.



How to adjust cushion

CAUTION

If the rotating speed is increased at the start of adjustment of the cushion, abnormal surge pressure will occur, and the rotary actuator or the machine may be damaged.

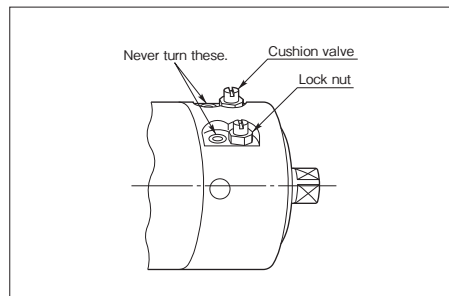
The cushion has been adjusted before shipment. However, since the cushion attenuation effect changes depending on the rotating speed and load inertia, adjust the cushion valve as stated below.

- Loosen the lock nut.
- Turn the cushion valve to the right or left to adjust the speed at the rotating end to reduce the shock and smoothen the operation. Turn the cushion valve to the right, and it will close. Turn it to the left, and it will open.

CAUTION

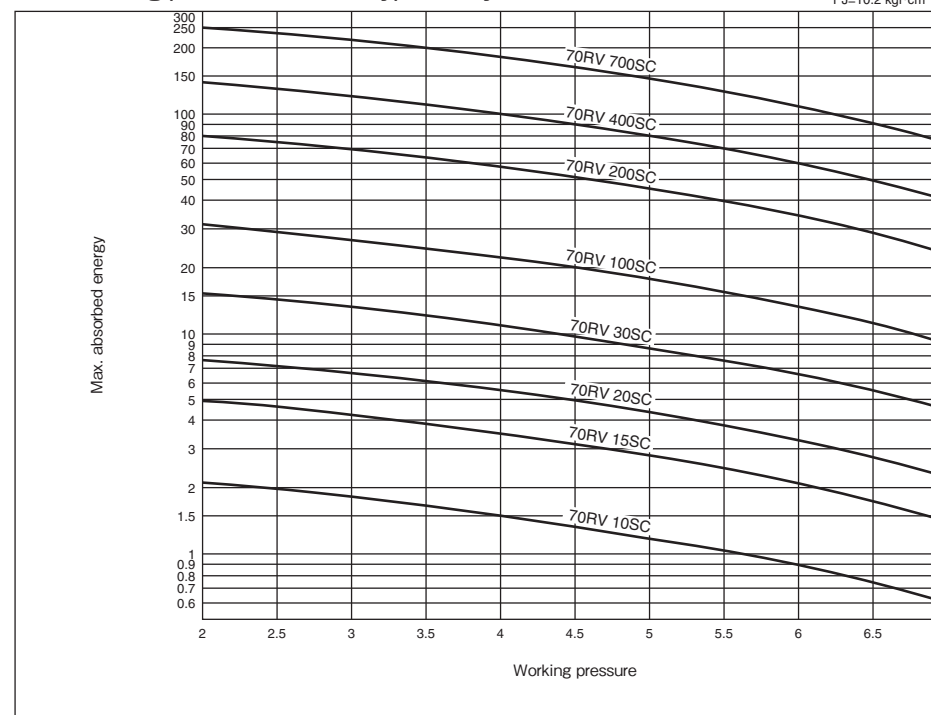
If the cushion plug is loosened excessively, the cushion valve may fly out or the fluid may spout out.

- After the completion of adjustment, secure the lock nut.
The energy which can be absorbed by the cushion is limited.
Adjust the cushion while gradually increasing the rotary actuator rotating speed from the state where the flow control valve is fully closed.
- The set screw beside the cushion valve is not designed to discharge air. Never turn it.



■ Dependence of max. energy absorbed by cushion on working pressure on vane type rotary actuator with cushion

1 MPa=10.2 kgf/cm²
1 J=10.2 kgf·cm



Control circuit

When using any vane type rotary actuator under light loading conditions, control the actuator with the basic circuit shown in Fig. 1. When using any vane type rotary actuator under heavy loading conditions, use a circuit as shown in Fig. 2, 3 or 4 to prevent application of shock and damage to the equipment due to surge pressure.

As aggressive measures to prevent shock and surge pressure, use a 2-stage deceleration control method as shown in Fig. 2, and adjust the deceleration time according to the loading conditions, reduction ratio, etc. As a control device for this purpose, use a pilot type switching valve or a proportional electromagnetic control valve.

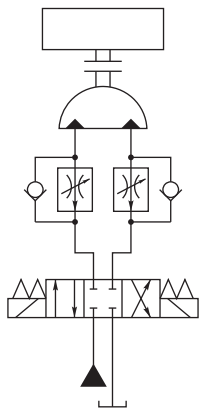


Fig. 1 (Basic circuit)

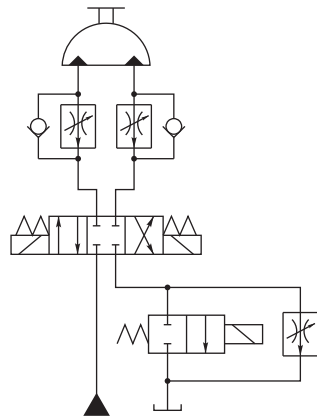


Fig. 2 (2-stage deceleration)

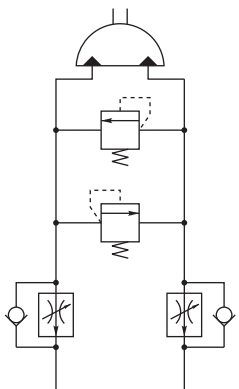


Fig. 3 (Brake valve)

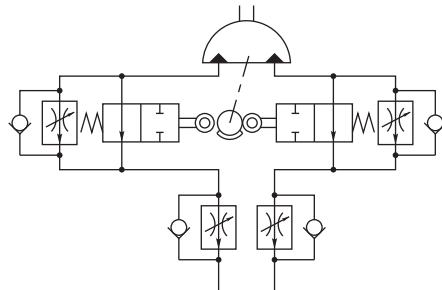


Fig. 4 (Deceleration valve)